

## Blazed Transmission Gratings for Constellation-X: EUV and Soft X-Ray Results

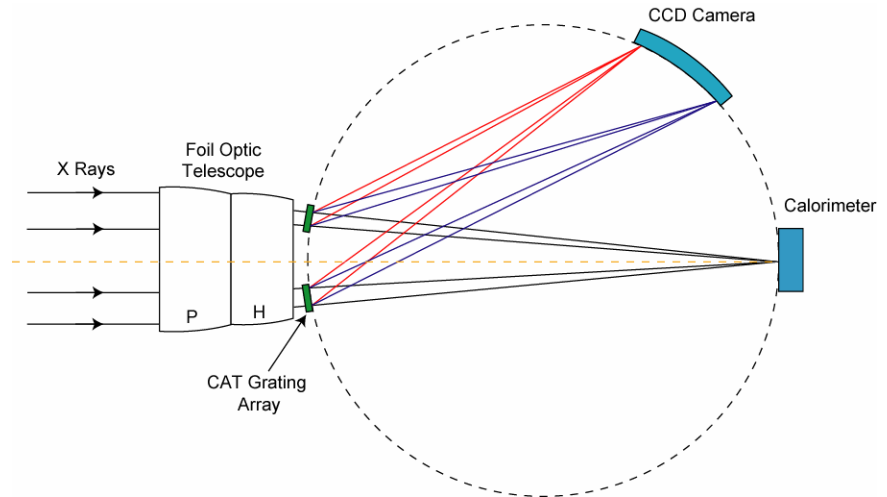
Ralf K. Heilmann, Minseung Ahn, and Mark L. Schattenburg

Constellation-X Facility Science Team Meeting  
Boulder, CO  
February 21, 2008

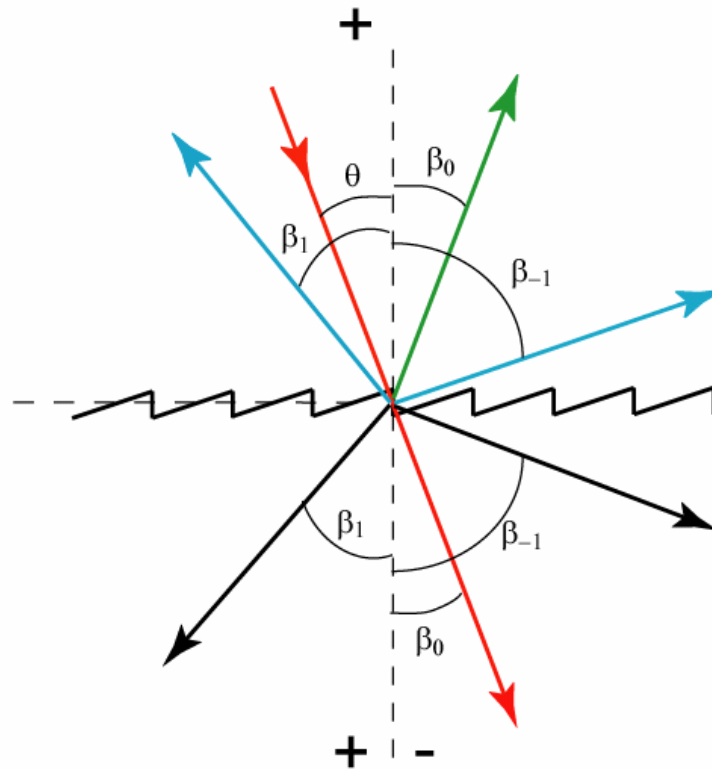
# Con-X CAT (Critical-Angle Transmission) Grating Spectrometer

Con-X requirements for effective area and resolution below 0.6 keV are met and exceeded by CATGS (Flanagan *et al.*, Dec.'06 FST and Proc. SPIE **6688**, 66880Y (2007))

- High efficiency blazed CAT gratings
- High resolving power ( $R=E/\Delta E > 2000$  (HEW) below 1.2 keV) due to high dispersion (10,000 lines/mm) and sub-aperturing
- High energy x-rays go to calorimeter at the telescope focus
- Effective area down to 165 eV
- Low mass (< 61 kg, incl. CCDs & electronics)
- Easy alignment tolerances (up to  $(m\lambda/p)^{-2} \sim 10^3$ - $10^4$  times better than reflection grating)

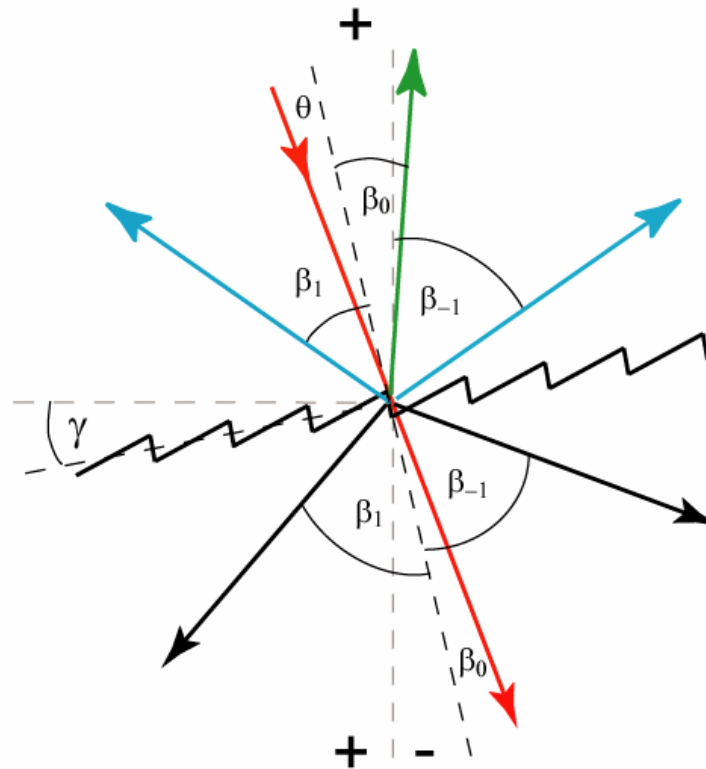


## Alignment sensitivity: Transmission Grating vs. Reflection Grating



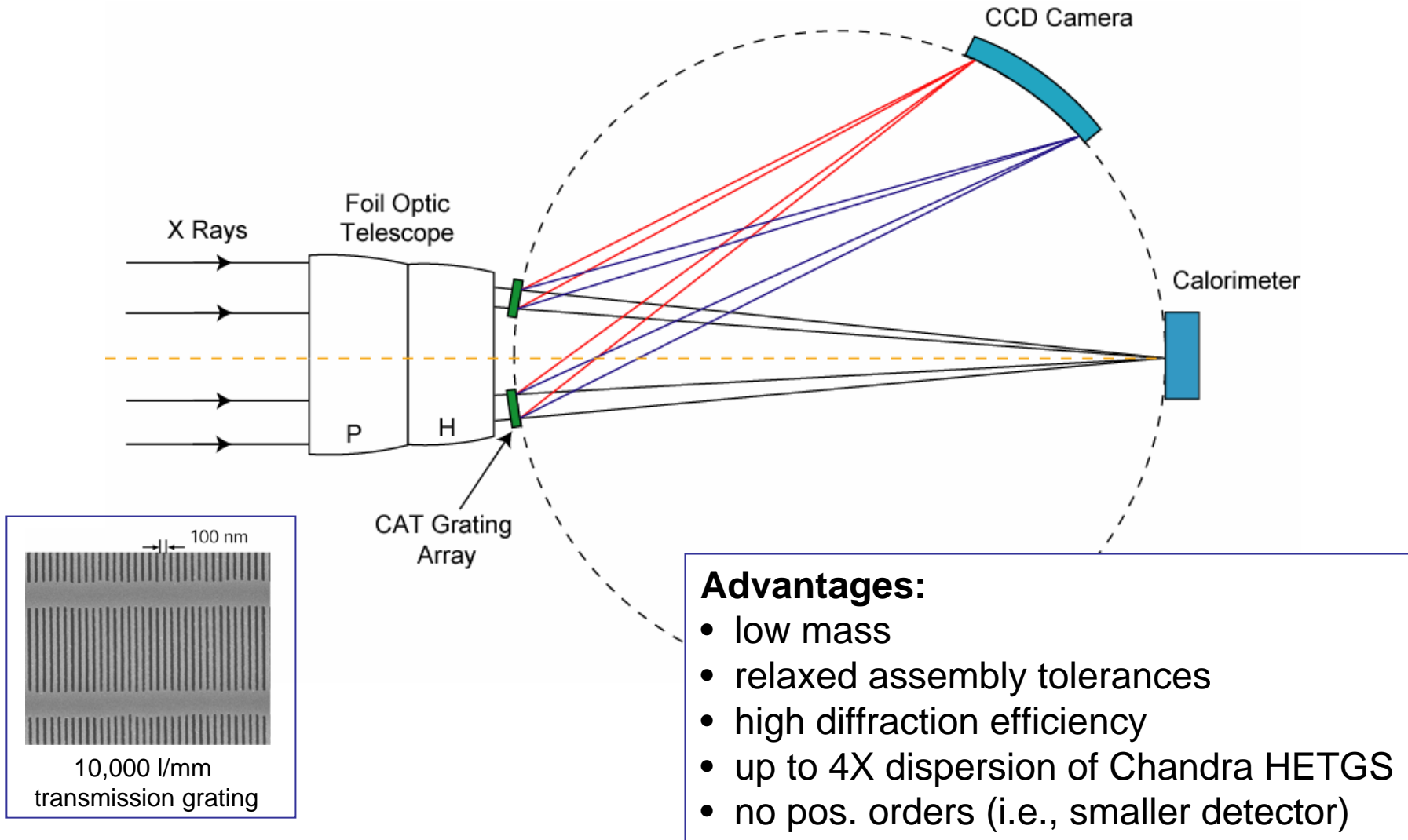
$$m\lambda/p = \sin\theta - \sin\beta_m$$

## Alignment sensitivity: Transmission Grating vs. Reflection Grating



$$m\lambda/p = \sin\theta - \sin\beta_m$$

# Con-X CAT (Critical-Angle Transmission) Grating Spectrometer Concept



# Con-X Critical-Angle Transmission Grating Spectrometer Layout

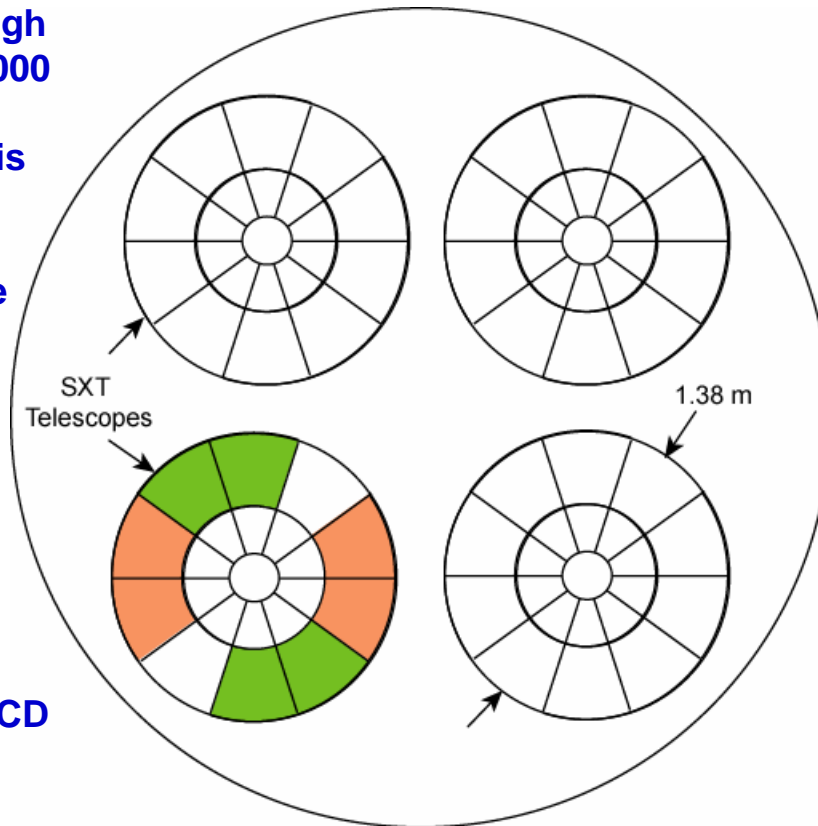
Two grating arrays are mounted on only one SXT. Each array has its own readout. The other 3 SXTs are unaffected.

Covers outer annulus  $R=324$  mm to 659 mm. Shells inward of the mirror gap are not covered to preserve high-energy throughput to the XMS.

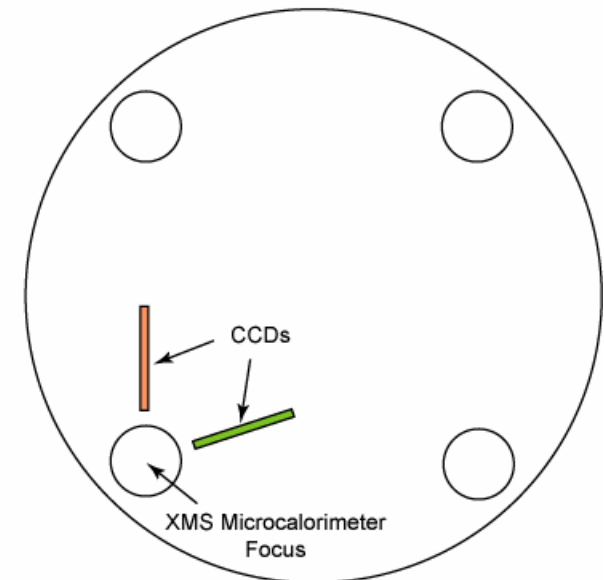
Gratings have high line density (10,000 l/mm) and are blazed: readout is compact and cleanly outside of XMS envelope

Readout range:  $m\lambda=25$  Å to 77 Å

Length 488 mm covered by 20 CCD devices (each)



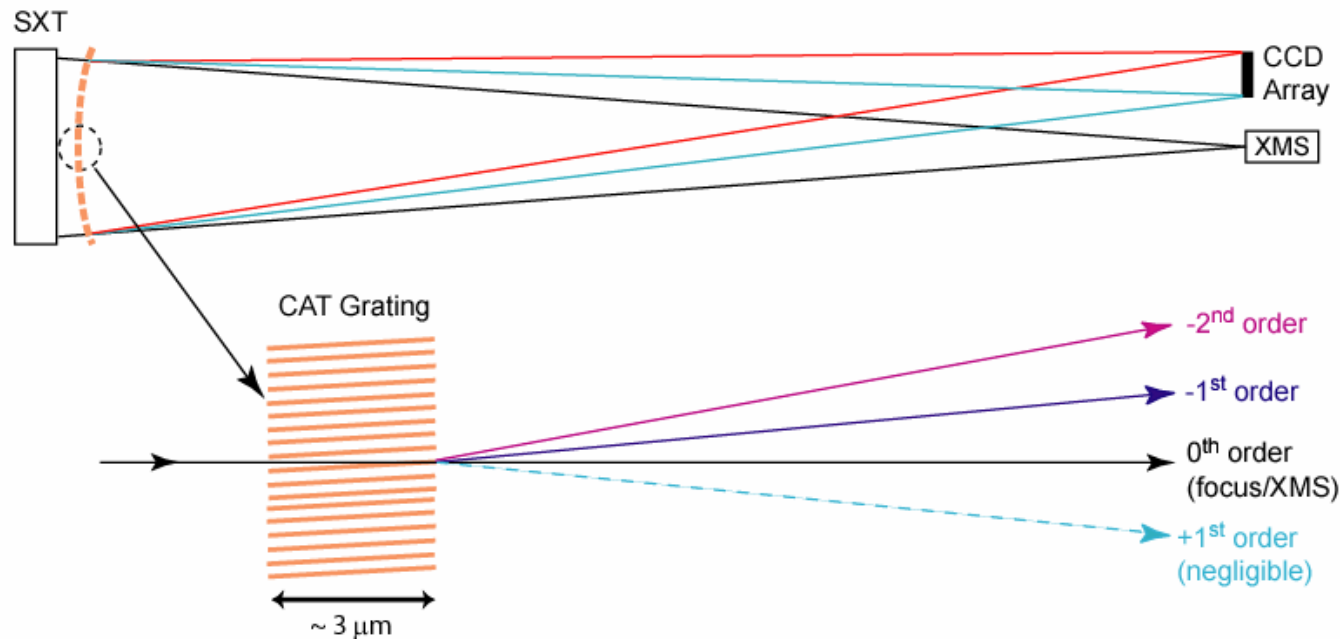
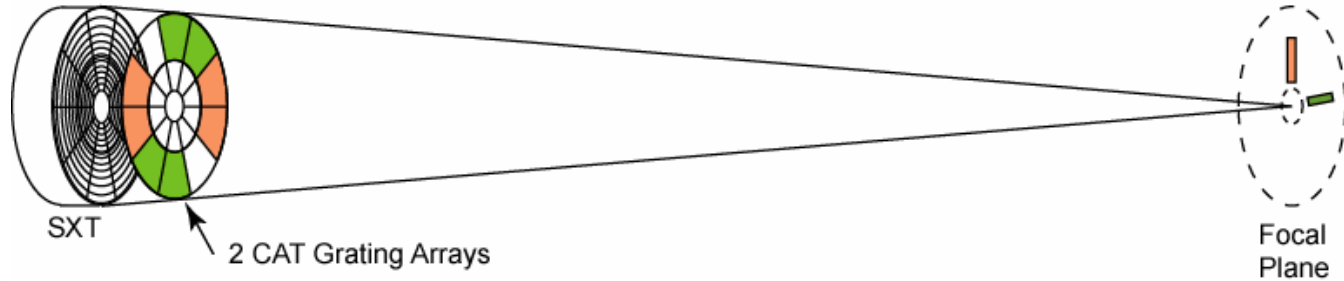
Mirror Bench View



Detector Bench View



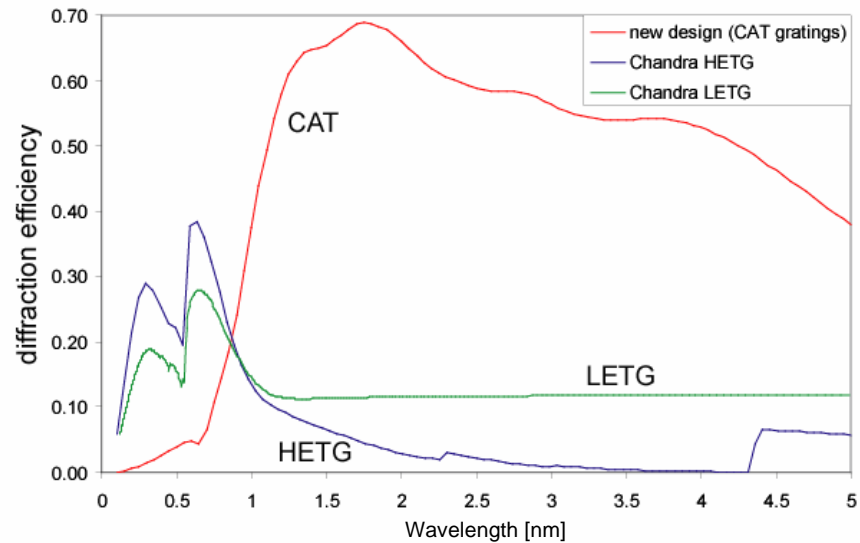
# CAT Grating Spectrometer (CATGS)



**Instrument is fixed in place and provides data for every observation, without interruption of any other instrument. The observer gets all the data, all the time.**

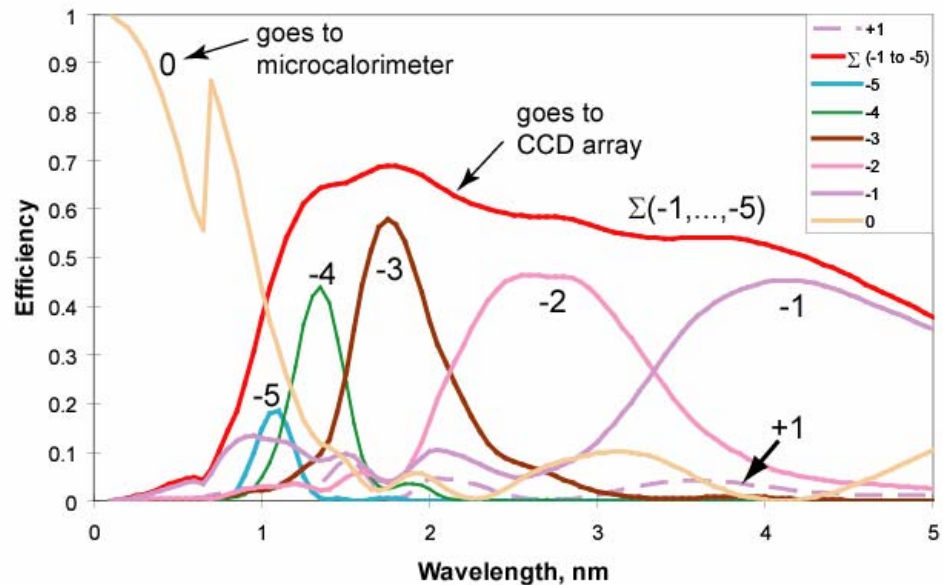
## Comparison of Grating Efficiencies:

### Chandra versus CAT Grating



### Predicted Silicon CAT Grating Diffraction Efficiency:

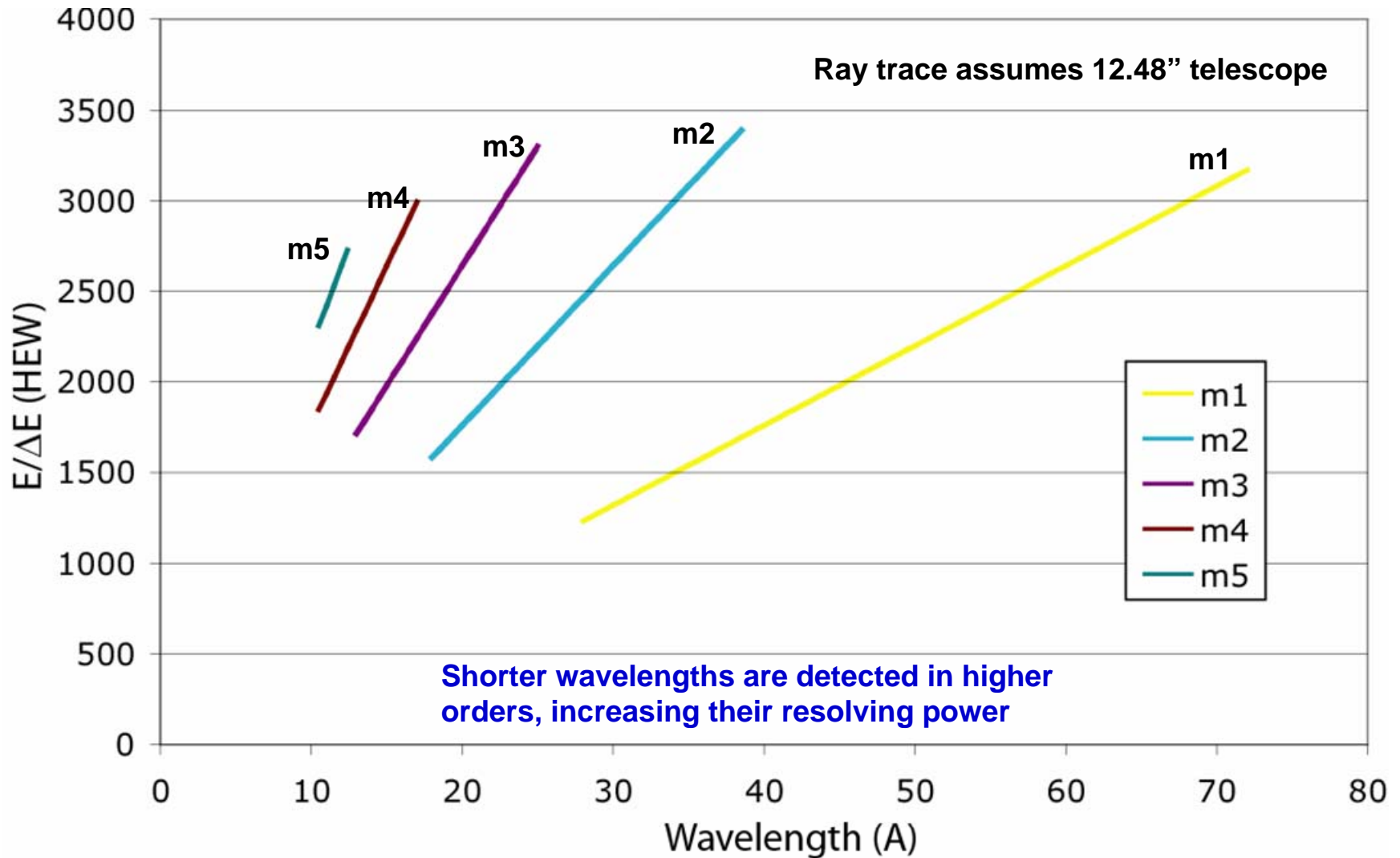
- Pronounced blazing
- High efficiency in 1<sup>st</sup> - 5<sup>th</sup> order: broad bandpass
- Little loss in 0<sup>th</sup> order (calorimeter) at shorter wavelengths



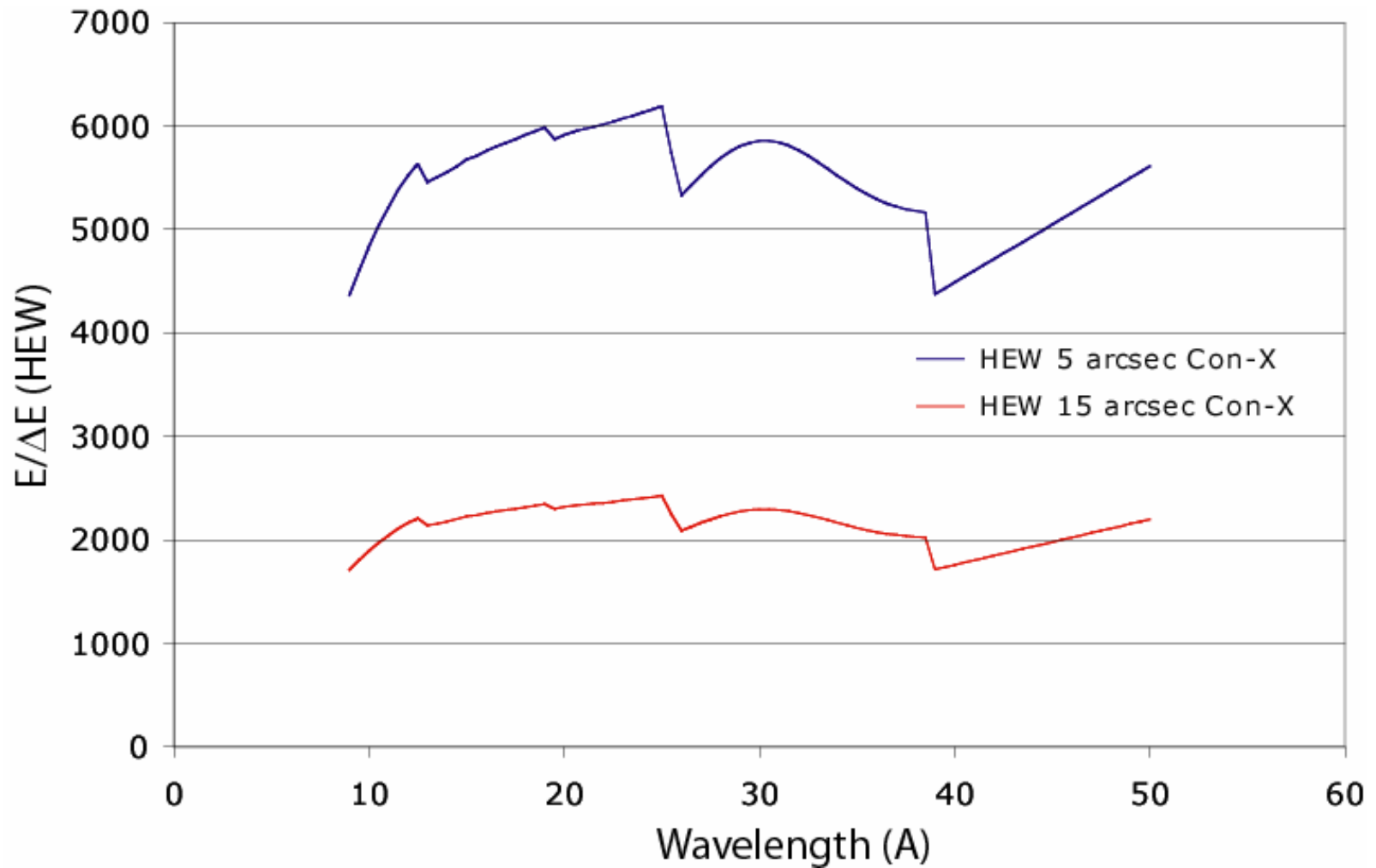


# Resolving Powers for Each Order

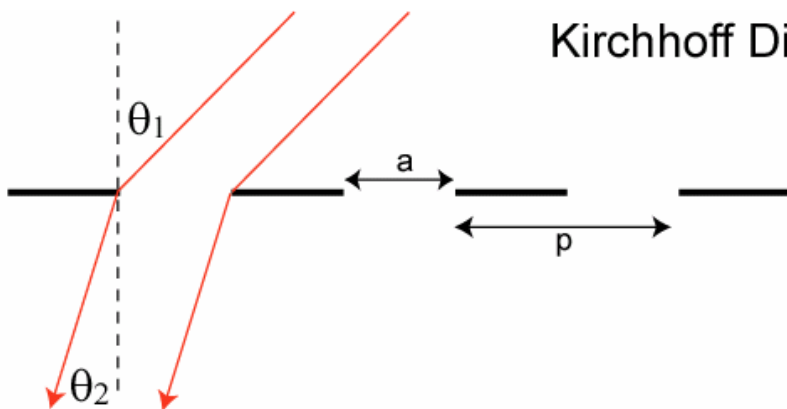
(where diffraction efficiency > 10%)



# Efficiency-Weighted Resolving Powers (HEW)



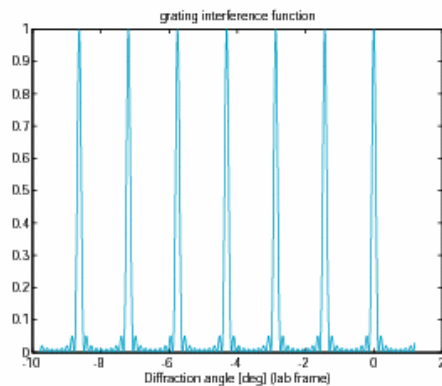
# Kirchhoff Diffraction Theory (Born & Wolf)



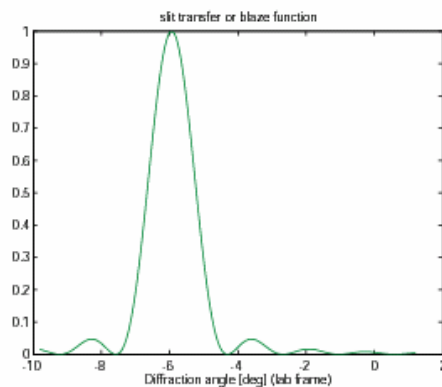
$$g = (\pi/\lambda) p (\sin\theta_2 - \sin\theta_1),$$

$$f = (\pi/\lambda) a (\sin\theta_2 - \sin\theta_1),$$

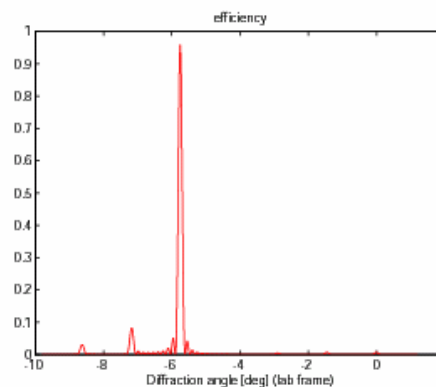
$n$  = number of slits



$$I_{\text{grat}} = (\sin(ng)/n \sin(g))^2$$



$$I_{\text{slit}} = (\sin(f)/f)^2$$



$$I_{\text{total}} = I_{\text{grat}} I_{\text{slit}}$$

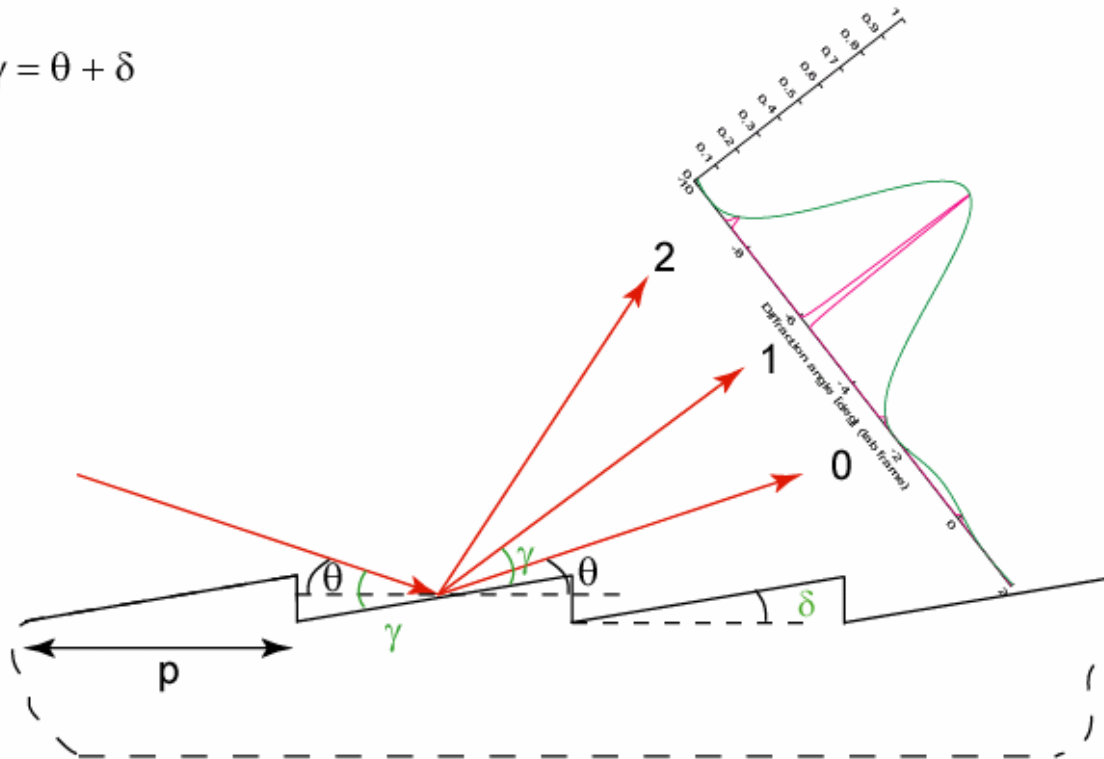
# Blazed Reflection Grating

$\theta$  – grazing angle of incidence relative to average grating surface

$\gamma$  – grazing angle of incidence relative to surface of single grating facet

$\delta$  – angle of facet relative to average grating surface

$$\gamma = \theta + \delta$$



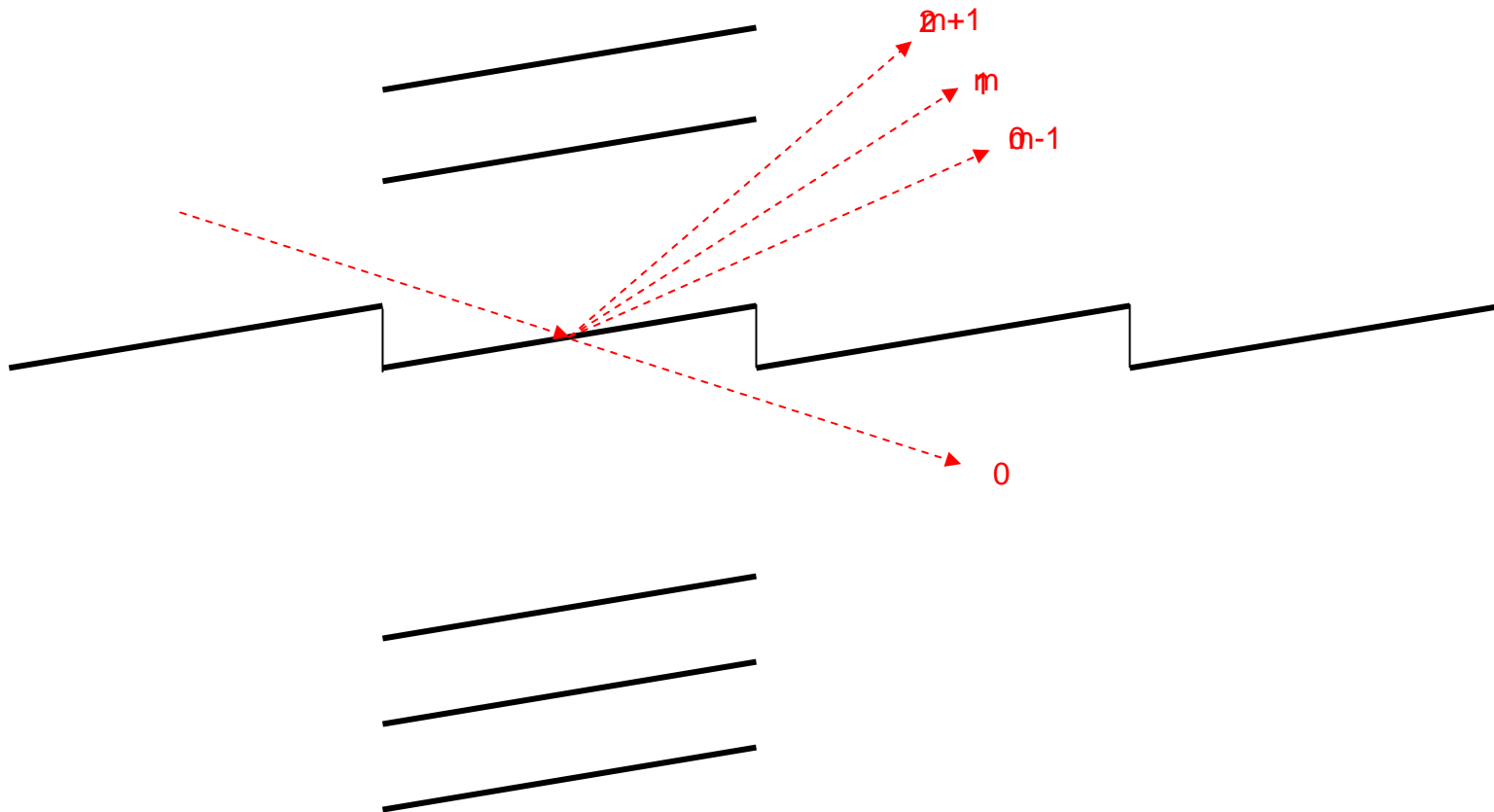
Diffraction angles  $\beta_m$ :

$$m\lambda/p = \cos \theta - \cos \beta_m$$

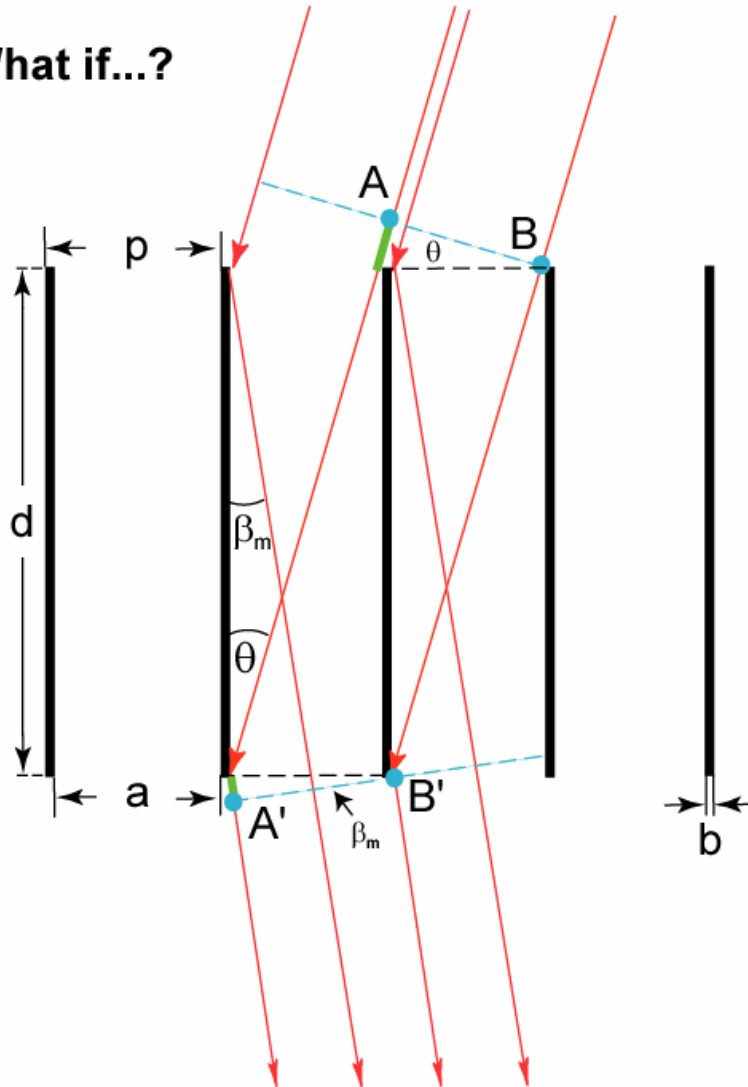
Diffraction intensities:

$$G(\lambda, p, \theta, \beta) * S(\lambda, a, \theta, \beta, \delta)$$

How do you go from a blazed reflection grating to a blazed transmission grating?



What if...?



Constructive interference when  
path length difference (PLD)  
between  $A'$  and  $B'$

$$\text{PLD} = p \sin(\theta) + p \sin(\beta_m) = m \lambda$$

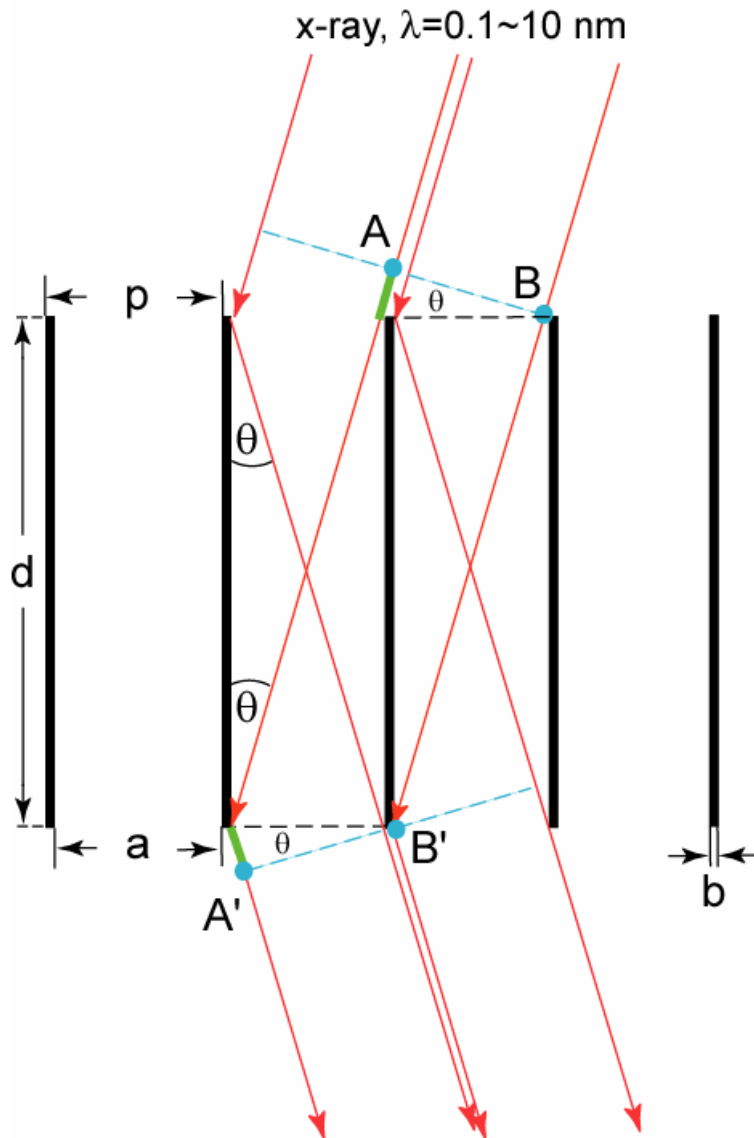
identical to Grating equation:

$$m \lambda = p (\sin(\theta) + \sin(\beta_m)),$$

with  $m$  = diffraction order



# Critical Angle Transmission (CAT) Grating



**Constructive interference when:**  
path length difference (PLD)  
between A' and B'

$$\text{PLD} = 2 p \sin(\theta) = m \lambda$$

**Blazing:** high diffraction  
efficiency when diffracted order  
coincides with specular  
reflection off of grating facet

**Refractive index and critical angle  
for x-ray and EUV :**

$$n = 1 - \delta + i\beta, \quad \delta \ll 1, \quad \beta \ll 1, \quad \beta \neq 0$$

$$\theta_c = (2\delta)^{1/2} : \sim 1 \sim 2^\circ$$

**High reflectivity when:**

$\theta < \theta_c$  , total external reflection

⇒ **Critical-Angle Transmission (CAT)  
Grating**

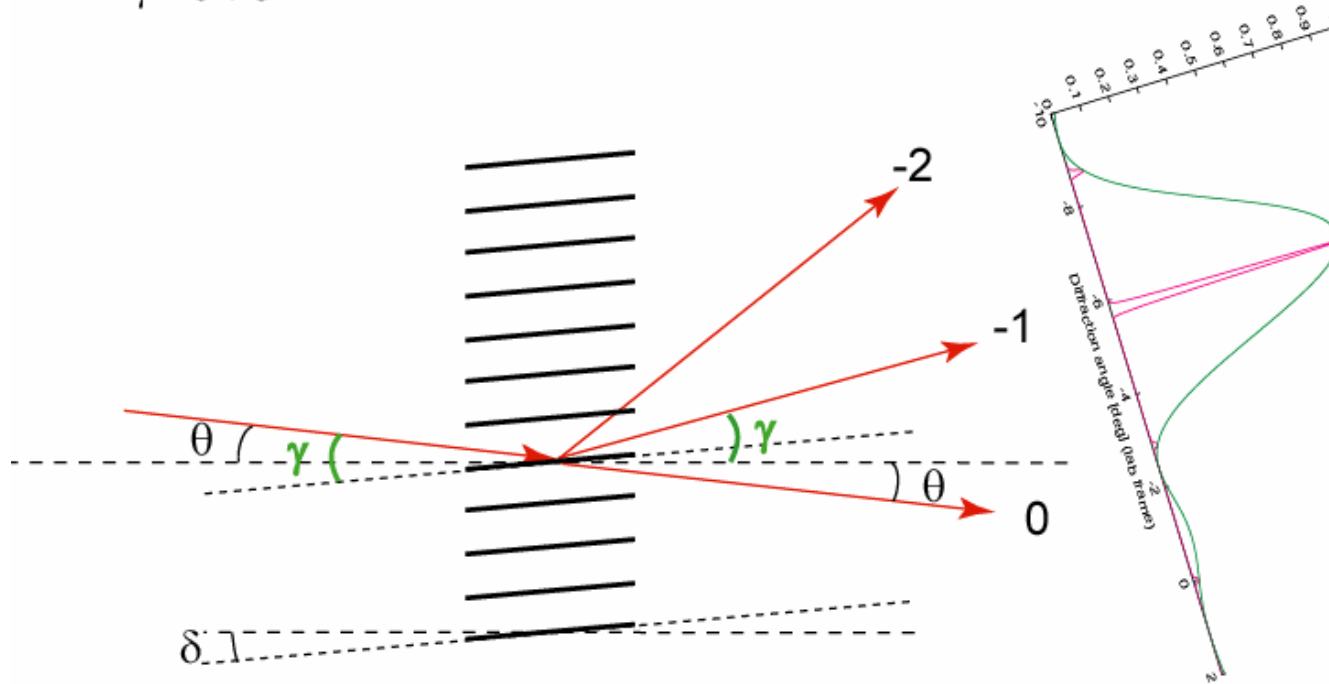
# Blazed Transmission Grating

$\theta$  – angle of incidence relative to grating normal

$\gamma$  – angle of incidence relative to surface of single grating facet (grating bar sidewall)

$\delta$  – angle of facet (sidewall) relative to average grating normal

$$\gamma = \theta + \delta$$



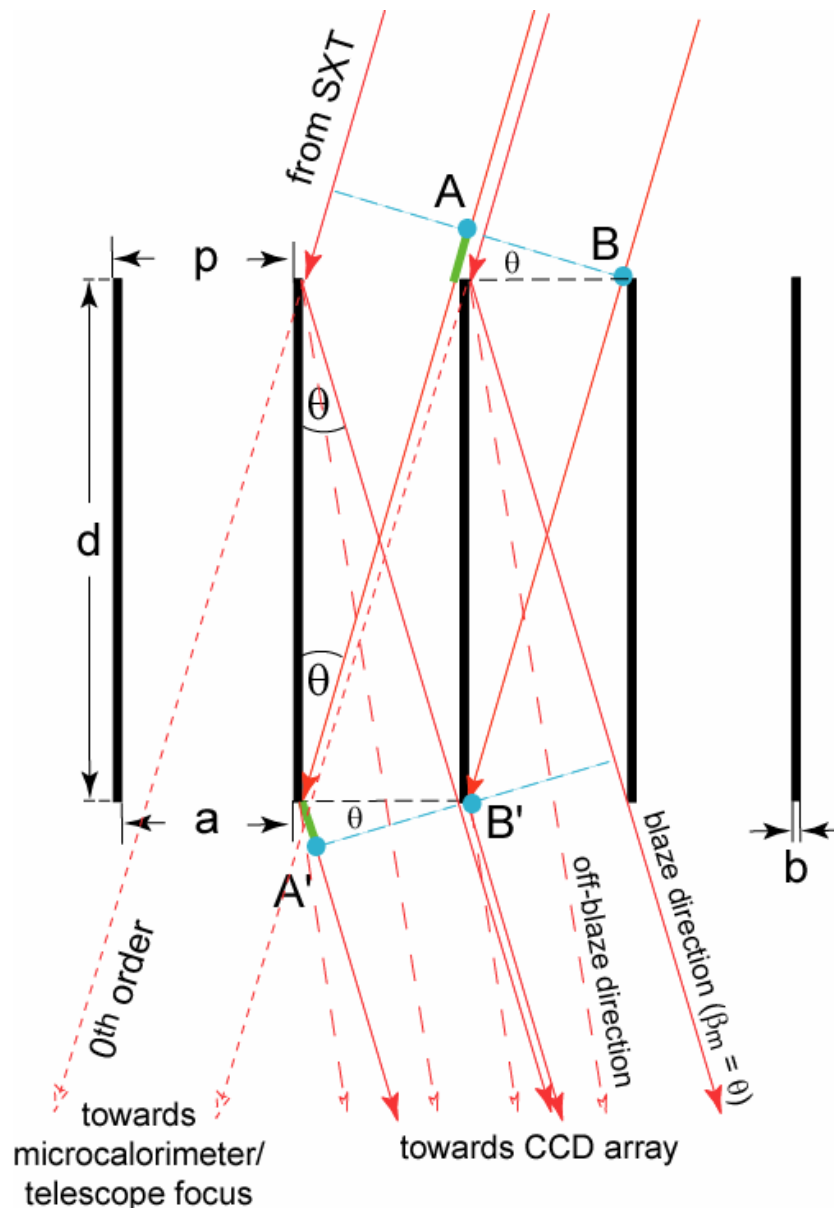
Diffraction angles  $\beta_m$ :

$$m\lambda/p = \sin \theta + \sin \beta_m$$

Diffraction intensities:

$$G(\lambda, p, \theta, \beta) * S(\lambda, a, \theta, \beta, \delta)$$

# Critical-Angle Transmission (CAT) Grating



**The CAT grating is a transmission grating, NOT a reflection grating!**

0th transmitted order (PLD = 0) consists of photons that are not deflected but penetrate the grating bars and go to the telescope focus. There is NO 0th order in the direction of specular reflection.

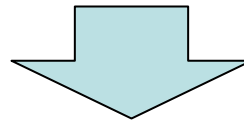
Diffraction is enhanced in the  $m^{\text{th}}$  order for wavelengths where  $\beta_m$  is close to  $\theta$ . Diffraction is strongly suppressed on the other side of the 0th order.

Rotation of the grating around the normal to the plane of incidence by a small angle  $\gamma$  results in a shift of the blaze condition relative to the incident beam by  $2\gamma$ , while the directions of the diffracted orders change by only  $\gamma$   $(m\lambda/p)^2 \sim \gamma m^2 \times 10^{-3} - 10^{-4}$ .

# CAT Grating Design Issues

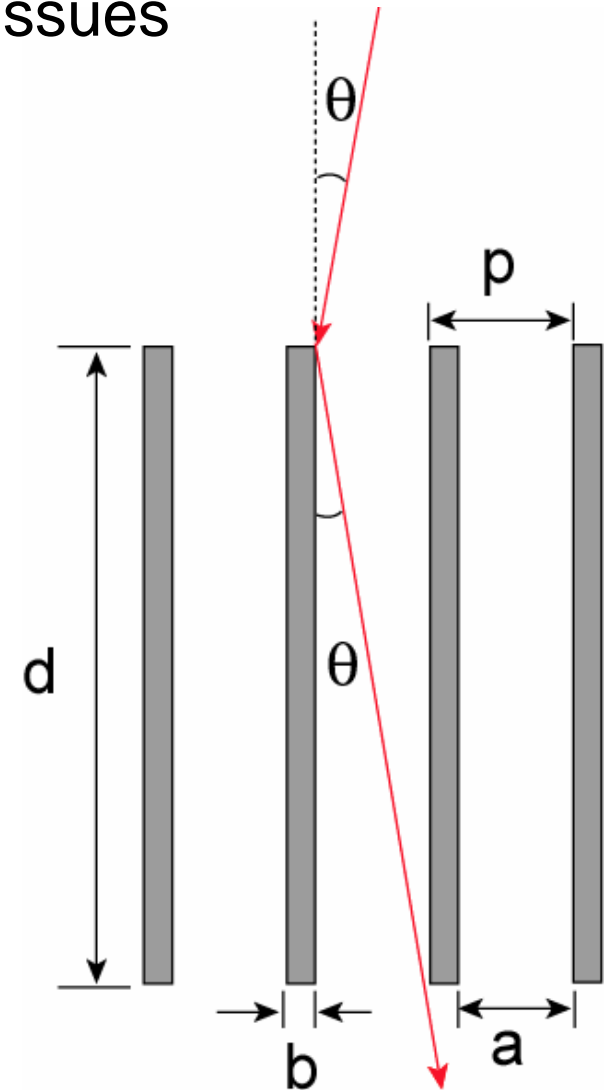
## Design Parameters (Con-X)

- Period,  $p = 100$  nm (larger dispersion)
- Duty cycle ( $b/p$ ) = 0.2 (high throughput)
- Critical angle,  $\theta = 1.5^\circ$  (high reflectivity)
- $d = a/\tan\theta = 3$   $\mu\text{m}$  (optimum “filling”)
- Sidewall roughness < 1 nm (high reflectivity)



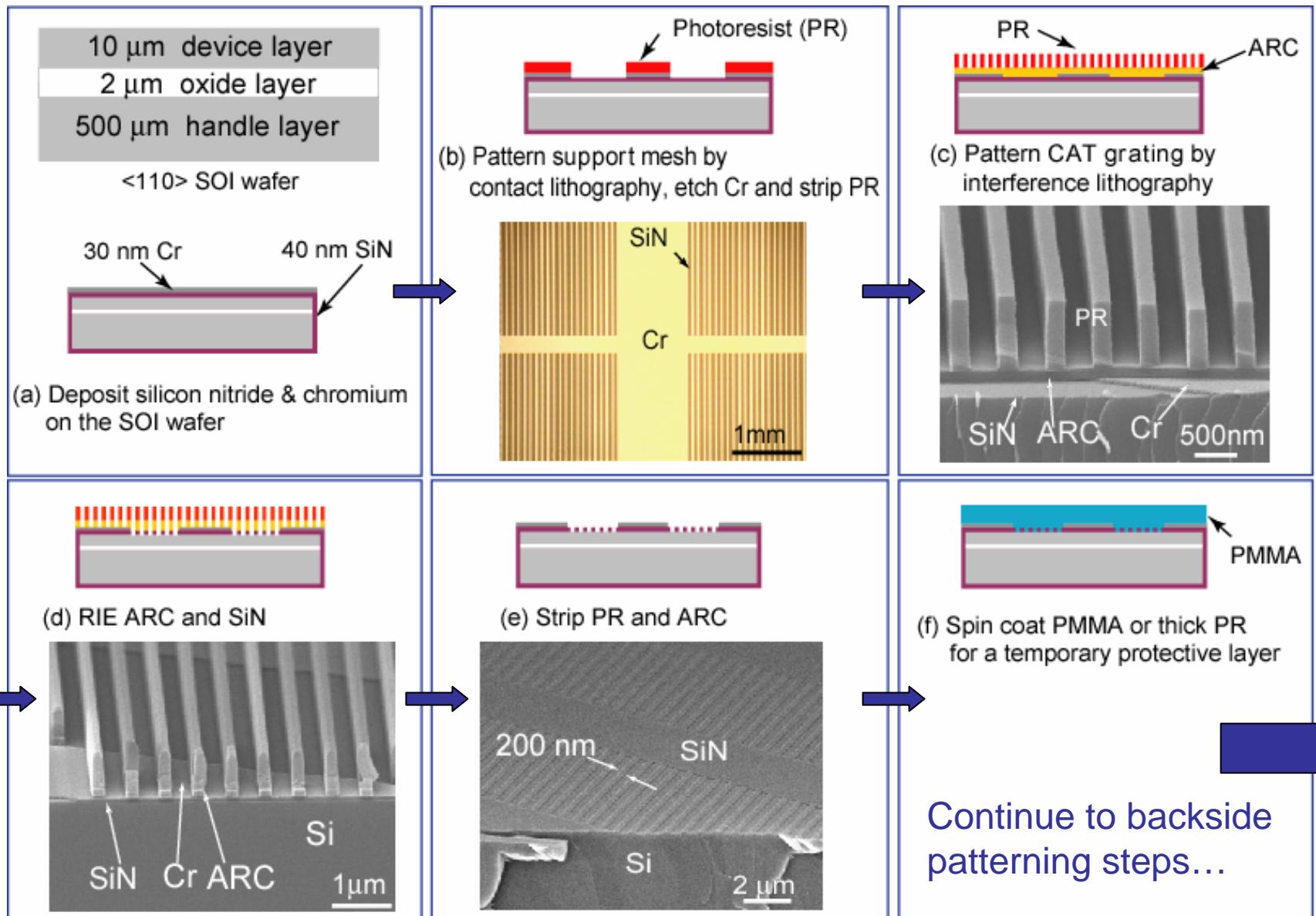
## Fabrication Challenges

- High aspect ratio ( $d/b \sim 150$ )
- Thin grating bars ( $b = 20$  nm)
- Freestanding structure
- Smooth sidewalls (roughness < 1 nm)
- Fine period gratings ( $p = 100$  nm)



Initial prototype:  $p = 574$  nm,  $d = 10$   $\mu\text{m}$

# Fabrication Process I. Front Side Patterning



# Fabrication Process II. Back Side Patterning



(g) Spin-coat PR on the back & contact lithography



(h) RIE SiN, strip PR and PMMA, and etch Cr



(i) Spin-coat the front with ProTEK\*



(j) TMAH etch & stop at oxide layer  
- 6 hours in 25% TMAH @ 90°C

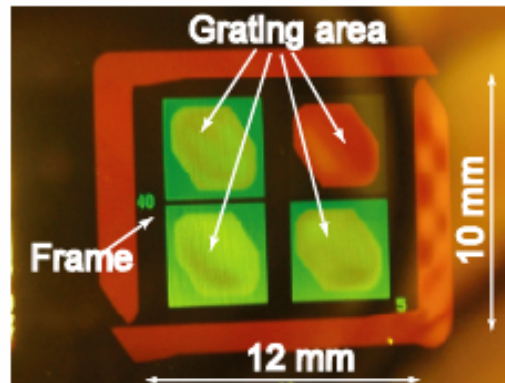


(k) Remove ProTEK by solvents and short plasma etching

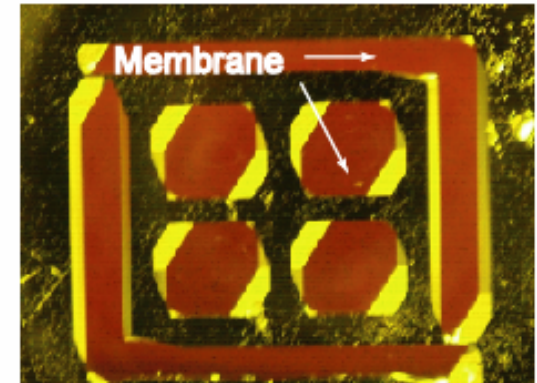
Continue to KOH etching...

\* ProTEK (Brewer Science Inc.) note:

- Protective polymer layer for base solutions such as KOH and TMAH
- ~10 hours in 35% KOH at 80°C
- Spin-coatable : 1~12  $\mu\text{m}$  thick
- Easy to remove : Solvent or  $\text{O}_2$  plasma



Top view



Bottom view



## Fabrication Process III. KOH Etching and HF Etching



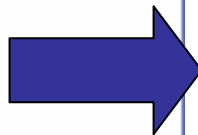
(l) BHF dip, KOH etch,  
stopped at buried oxide

- High KOH concentration: 50 wt%
- Low temperature: 50 °C
- Etch rates:  $R_{\langle 110 \rangle} \approx 185 \text{ nm/min}$   
 $R_{\langle 111 \rangle} \approx 1.49 \text{ nm/min}$
- Anisotropy ( $R_{\langle 110 \rangle} / R_{\langle 111 \rangle}$ ) = 124



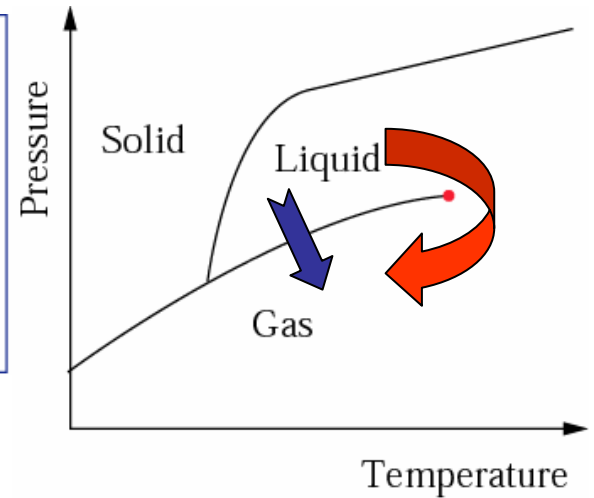
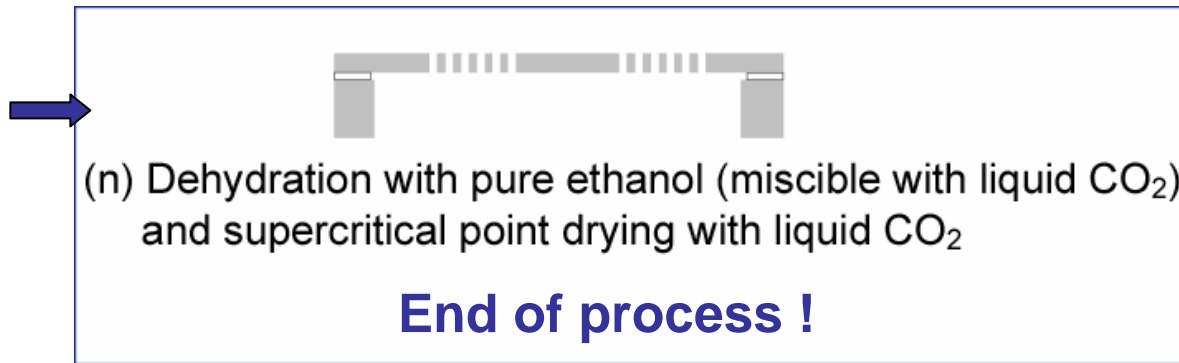
(m) HF etch buried oxide  
and SiN mask

- 5 min in 48 % HF
- Membrane ripples ( $\text{SiO}_2$  stress) disappear

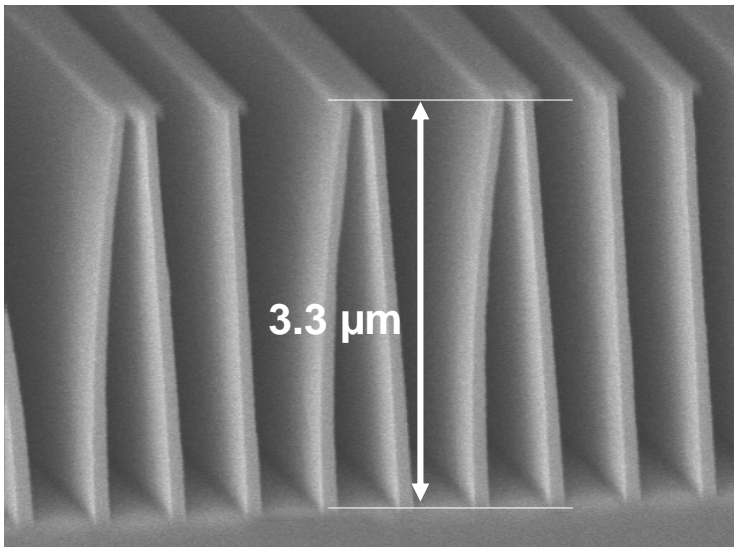


Continue to  
drying step...

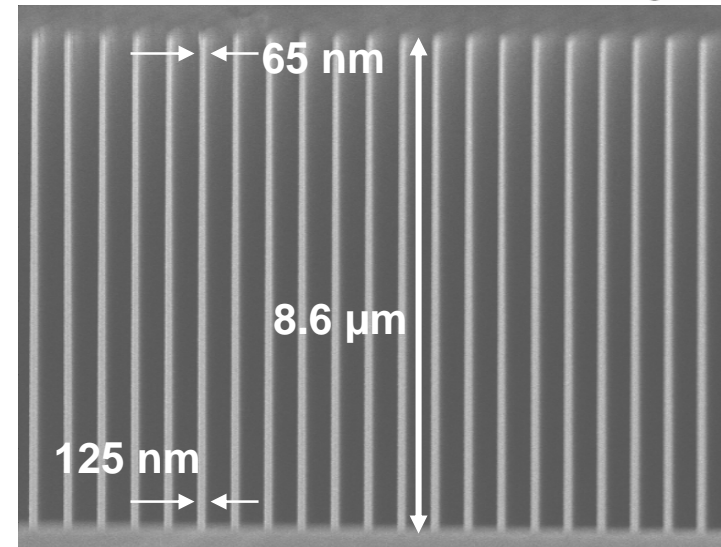
# Fabrication Process IV. Supercritical Drying



- Stiction problem for high aspect ratio structures



**Air dried, aspect ratio ~ 20**

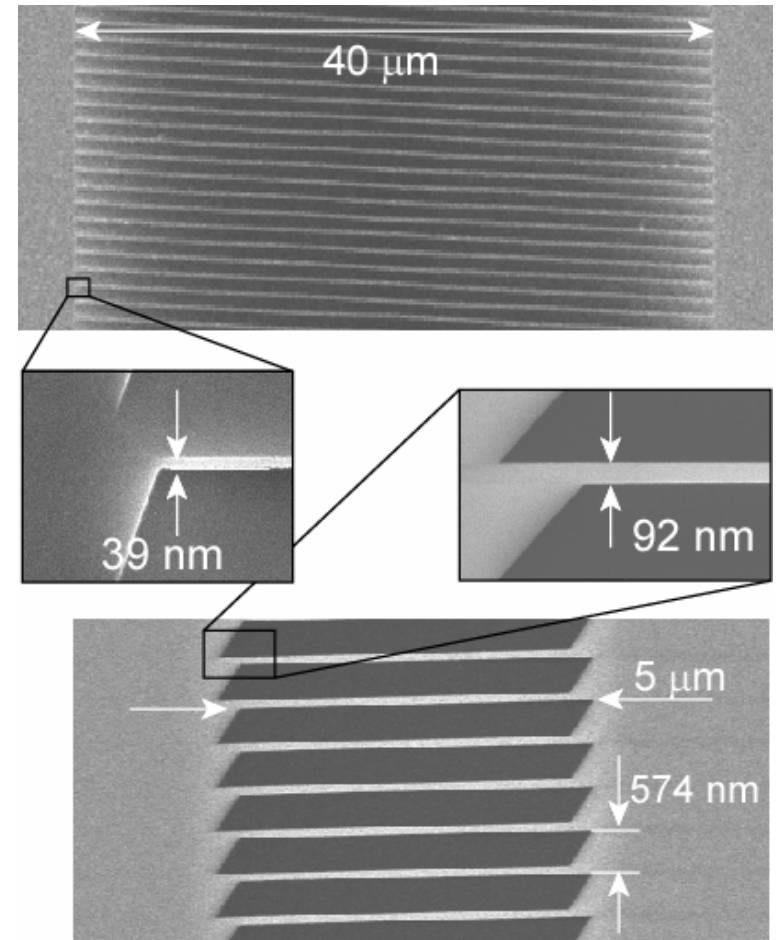
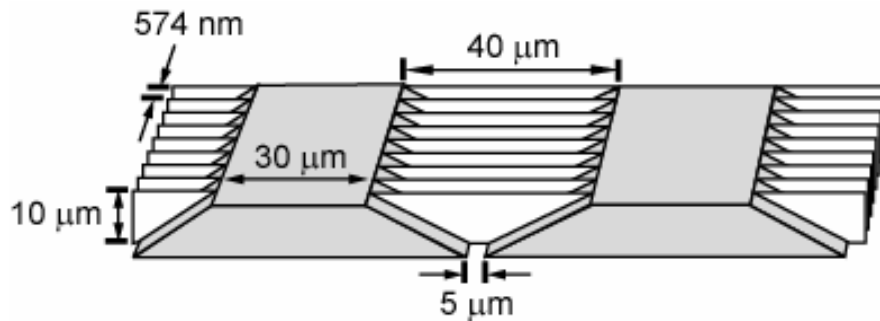


**Supercritical drying, aspect ratio ~ 100**

# Critical Angle Transmission (CAT) Grating Prototype

Period  $p = 574 \text{ nm}$   
Depth  $d = 10 \text{ }\mu\text{m}$   
Duty cycle  $(b/p) = 0.15$   
Aspect ratio  $(d/b) > 115$

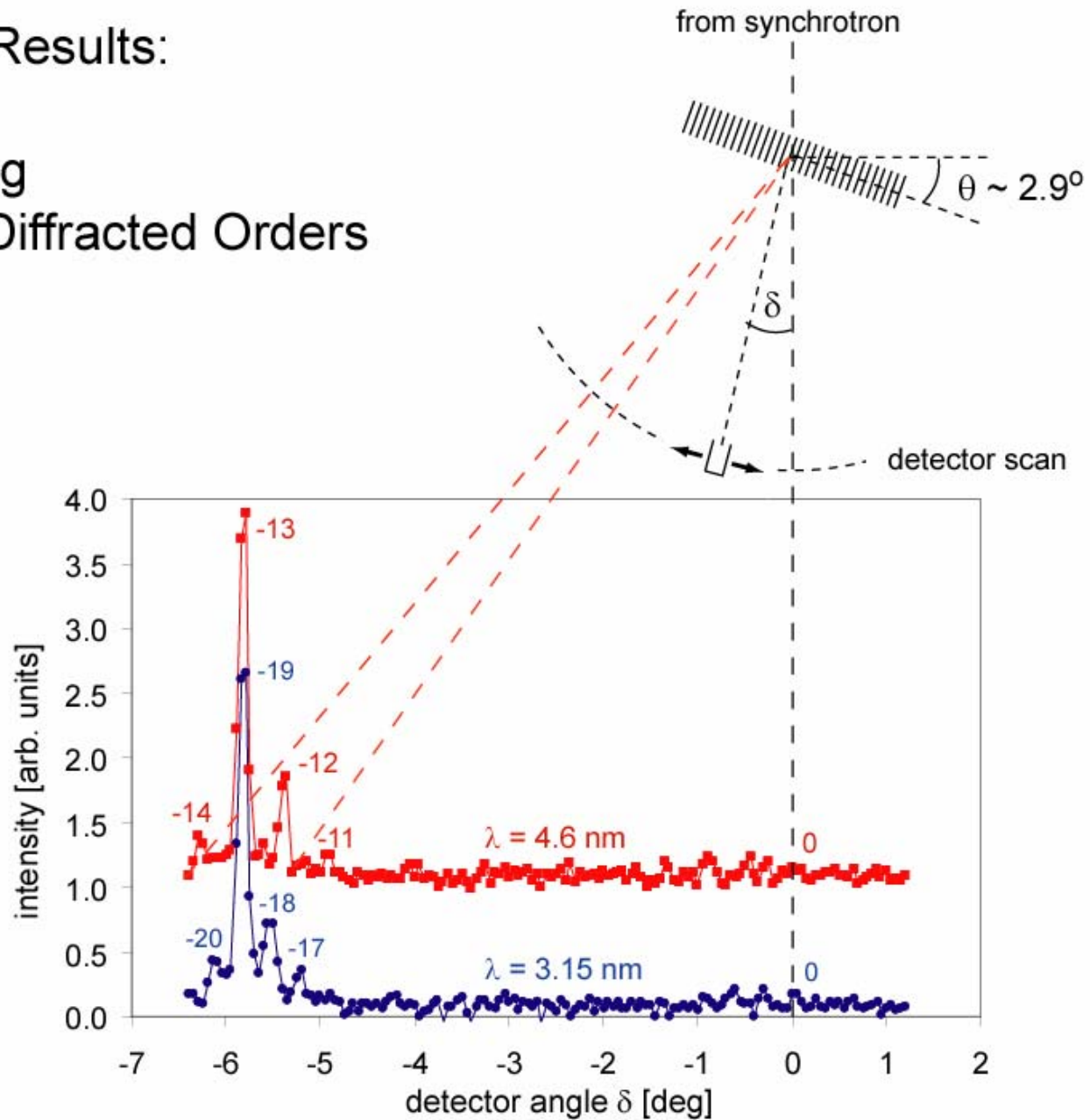
Support bar width =  $30 \text{ }\mu\text{m}$   
Support period =  $70 \text{ }\mu\text{m}$



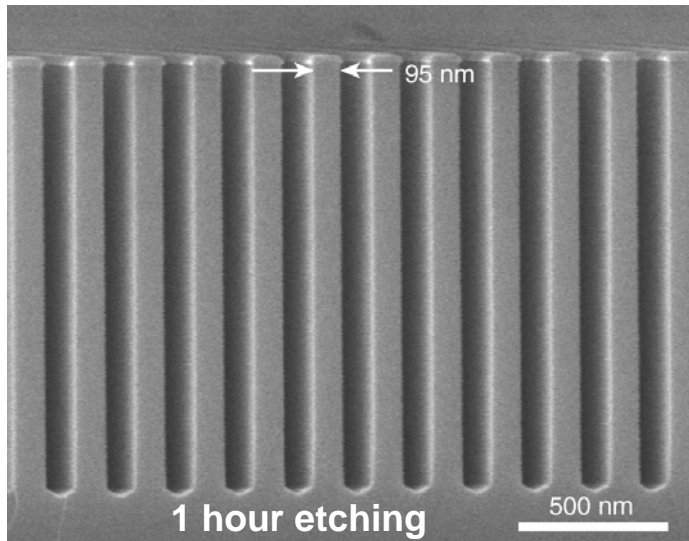
Ahn *et al.*, JVST B **25**, 2593 (2007)

# X-Ray Results:

- Blazing
- High Diffracted Orders



# 200 nm-period CAT grating fabrication with improved process



**$\langle 110 \rangle$  vertical etch rate = 1.4  $\mu\text{m/hr}$**

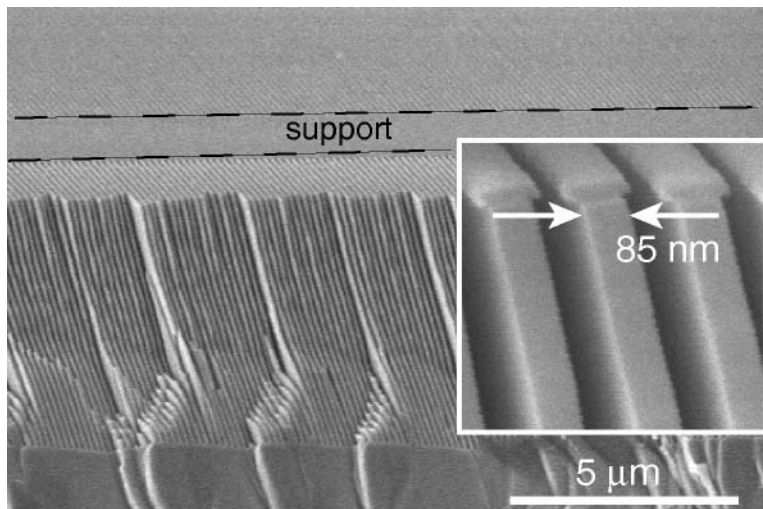
**$\langle 111 \rangle$  lateral etch rate = 1.25 nm/hr**

**Record Etch Anisotropy**

**$(R_{\langle 110 \rangle} / R_{\langle 111 \rangle}) = 500 \sim 1000$  (!!!)**

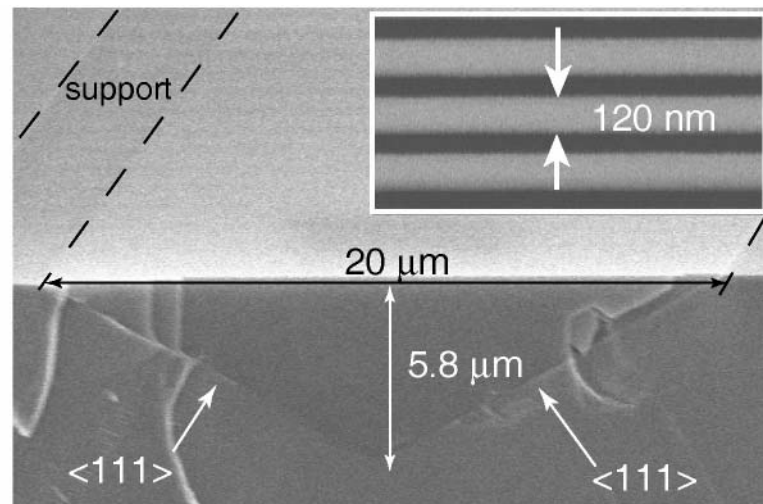
**allows long over-etching  $\Rightarrow$**

**increased process latitude & uniformity**



(a)

5 hour etching and critical point dried



(b)



# Summary

- Transmission Grating Spectrometer with Critical-Angle Transmission (CAT) gratings meets/exceeds all Con-X mission requirements.
- Fabricated freestanding CAT grating prototype that meets milestones for aspect ratio, duty cycle, and sidewall roughness.
- Experimentally demonstrated CAT grating principle of operation in the EUV and soft x-ray band with high diffraction efficiency.
- Introduced numerous fabrication process improvements.
- Fabrication of 200 nm-period CAT gratings near completion.
- Next:
  - X-ray tests of 200 nm-period CAT gratings.
  - Increase open area fraction.
  - Develop and optimize integrated support mesh and back-side support for increased mechanical strength and larger grating areas.



# Acknowledgments

- NASA ROSES funds
- Kathryn Flanagan (STScI)
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